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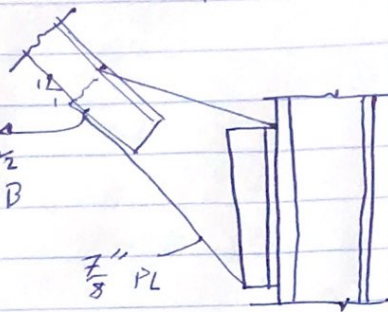
Part 3

Q.7 A36 Steel
double angle

$$D_s = 35 \text{ in}$$

$$L_s = 105 \text{ in}$$

2 L5 x3 x 1/2
LL BB



Gusset Plate: thickness = $\frac{7}{8}$ "

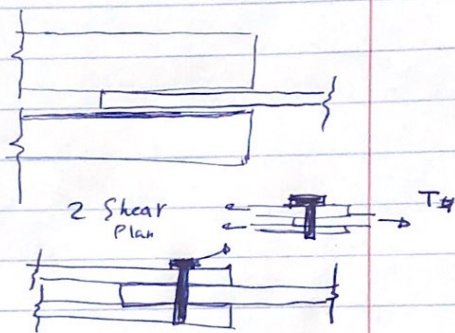
$\frac{3}{4}$ " A325-N bolts

including
threads
in Shear Plane

$$F_y = 36 \text{ ksi}$$

$$F_u = 58 \text{ ksi}$$

Top view:



$$T_u = 1.2D + 1.6L = 210 \text{ k}$$

Bearing type Conn. ϕ for one bolt:

$$\phi R_n = 0.8 [0.75 F_{nv} A_{bolt}] = 17.3 \text{ k/bolt}$$

from Table J3.2 $\Rightarrow F_{nv} = 48 \text{ ksi}$

$$A_b = \frac{d^2 \pi}{4} = 0.6 \text{ in}^2$$

$$\# \text{ of bolts} = \frac{T_u}{\phi R_n} = \frac{T_u/2}{\phi R_n} = \frac{210/2}{17.3} = 6.07 \text{ bolts} \Rightarrow 7 \text{ bolts}$$

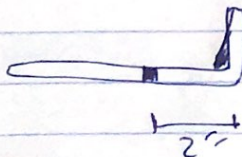
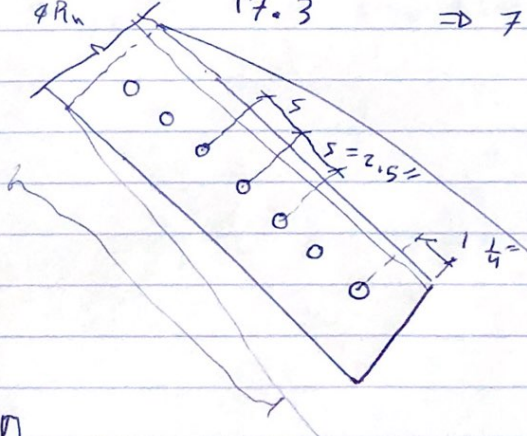
$$S_{min} = 2 \frac{2}{3} d_{bolt}$$

$$= 2.33 \text{ in}$$

$$S = 2.5 \text{ in}$$

edge distance from J3.4:

$$S' = 1 \frac{1}{4} \text{ in}$$



check for ~~stress~~

connected parts:

for bolt Bearing: $\phi R_n = 0.75 (2.4 d t F_u) = (0.75)(2.4) \left(\frac{7}{8}\right)^2 (58)$
(interior): $= 79.9 \text{ k}$

Tear out: $\phi R_n = 0.75 (1.2 L_c t F_u)$

$L_c = 2.5 - \frac{7}{8}$
 $= 1.625$

$= 74.2 \text{ k}$

$\phi R_n = 74.2 \text{ k} > T_{\text{from bolt}} = R_u = \frac{210/2}{7_{\text{bolt}}} = 15 \text{ k}$

ϕR_n from two angles $= \phi R_n (2) (0.9) f_y A_{\text{for angle}} = 243 \text{ k}$
 3.75 in^2

for bolt Bearing: $\phi R_n = 79.9 \text{ k}$

exterior Tear out: $\phi R_n = (0.75) (1.2) (1.25 - \frac{7}{8}) (7/8) (58)$

$= 37 \text{ k} > T = 15 \text{ k}$

No Problem.

$\phi R_n > R_u$
diagonal

$243 \text{ k} > 210 \text{ k}$